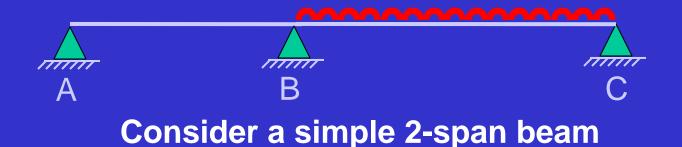
This is an alternative method to the slope-deflection method for analysing statically indeterminate planeframe structures

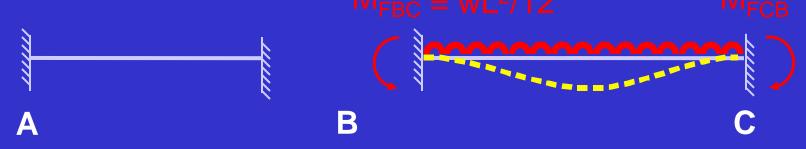
The method is suitable for frame elements, where the principal deflection effects are caused by bending rather than shear or axial loading

The method makes use of the Principle of Superposition, fixed end moments and the slope-deflection equations

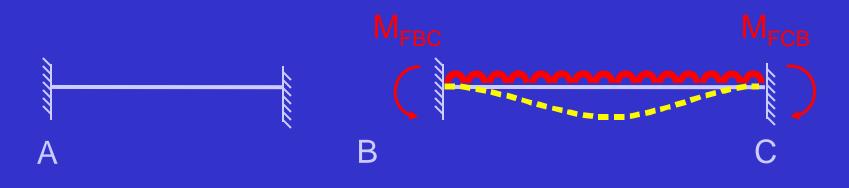
It is an iterative process that converges on an equilibrium solution...easier for hand calculations than the slope-deflection method



First fully fix the ends of members AB and BC and apply the loading.



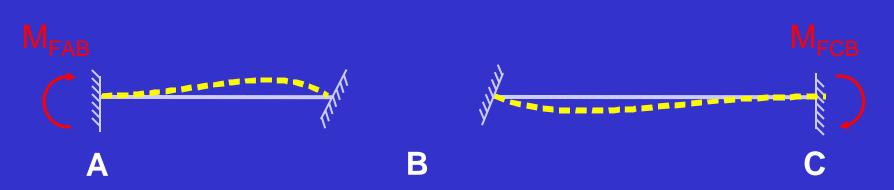
Hence find the fixed-end moments



Joint B in this example wants to rotate in a clockwise direction but cannot.

Joint B is not in equilibrium. $M_{BA} = 0$ but $M_{BC} = M_{FBC}$.

The joint is out of balance

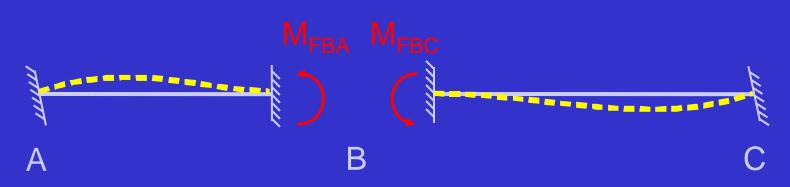


If we now release the fixity at Joint B and allow it to rotate then equilibrium is restored at this joint. The joint is balanced.

However this rotation now causes additional moments to the transferred to joints A and C, which are still fixed.

These moments are known as carry-over moments

The beam is still not in equilibrium... joint A and joint C would both like to rotate anti-clockwise, but cannot because they are fixed.



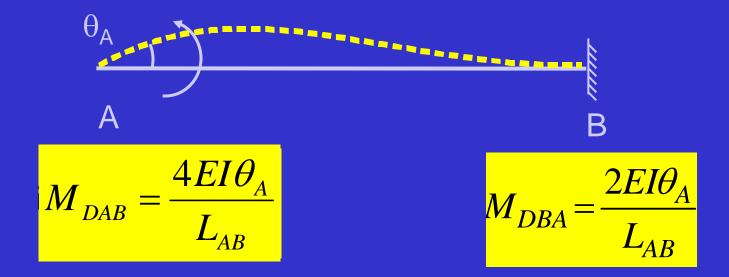
If we now fix joint B, and allow rotations at joints A & C (not the same rotation)

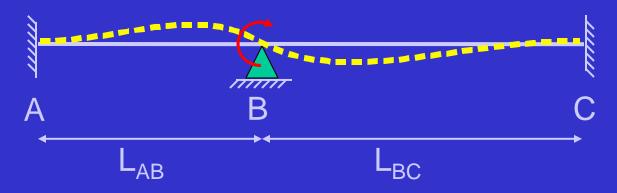
Then new carry-over moments are transferred back to joint B

If the moments at joint B do not balance each other, then we must again fix joints A & C and allow joint B to rotate. We continue with this and the carry-over moments will get smaller and smaller with each rotation until equilibrium is restored throughout

Stiffness, carry-over moments and distribution factors

When a joint is released and allowed to rotate, the out of balance moment must be shared between the members on each side of the joint according to the bending stiffness of each member. If we force a positive (anticlockwise) rotation θ_A .

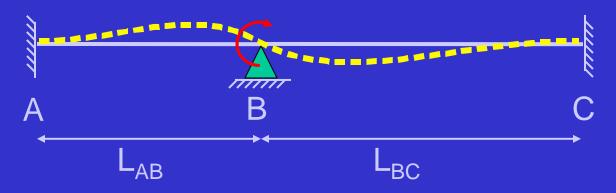




When joint B rotates by an angle θ_B , there are moments induced in AB and BC at B according to the bending stiffnesses of AB & BC.

These are known as the balancing moments

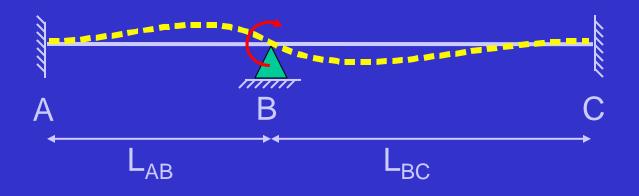
$$M_{DBA} = \frac{4EI\theta_B}{L_{AB}} \qquad M_{DBC} = \frac{4EI\theta_B}{L_{BC}}$$



Thus equilibrium is restored to an out of balance joint by rotating the joint and adding moments to either side of the joint according to the rotational stiffness of the member on each side.

$$M_{DBA} = M_{O-O-B} \times \underbrace{\frac{1}{L_{AB}}}_{1L_{AB}} + \frac{1}{L_{BC}} M_{DBC} = M_{O-O-B} \times \underbrace{\frac{1}{L_{BC}}}_{1L_{AB}} + \frac{1}{L_{BC}}$$

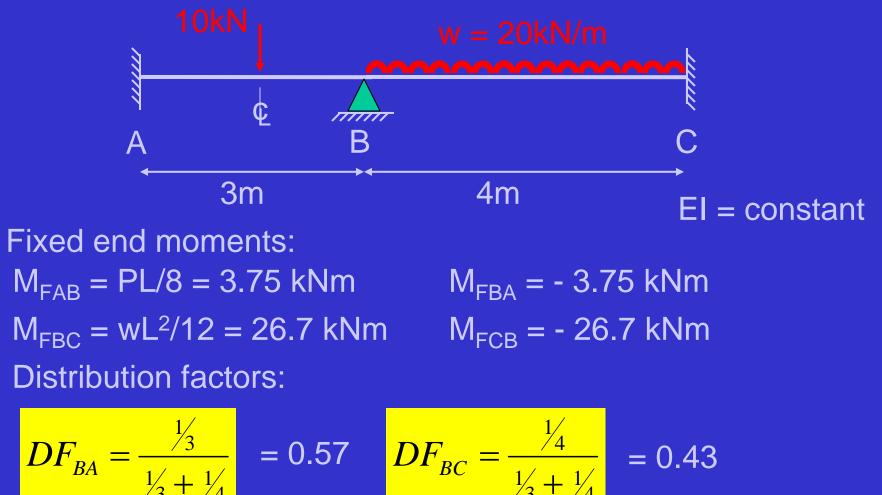
For constant EI Distribution factor



Half of the balancing moment is carried over to the joint at the other end of the member

$$M_{DAB} = \frac{M_{DBA}}{2} \qquad M_{DCB} = \frac{M_{DB}}{2}$$

So ... now we are ready to try a numerical example:

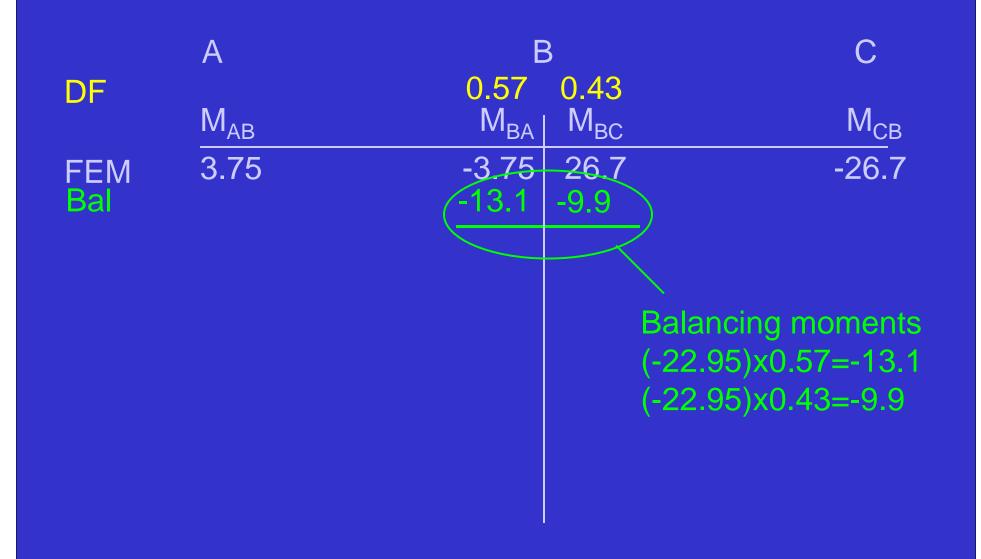


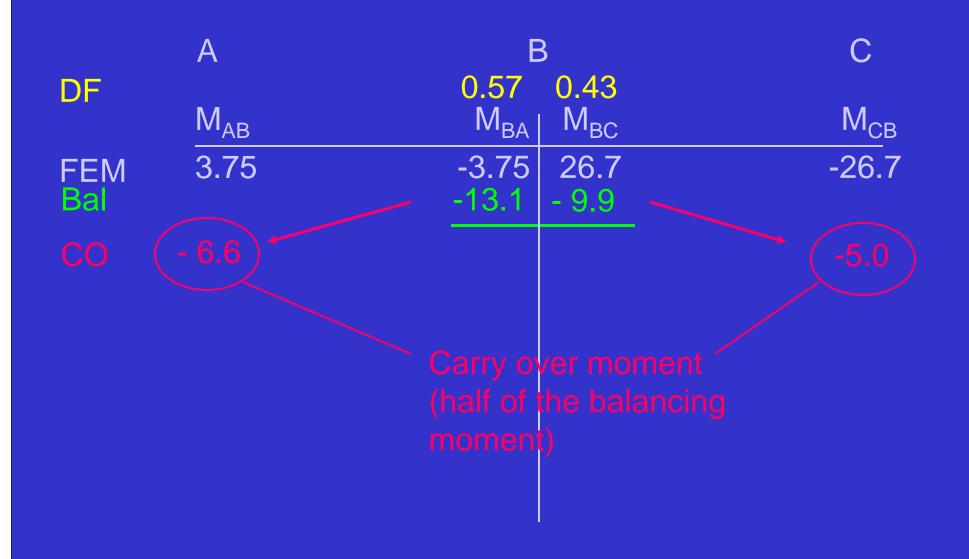
Carry out calculations using a moment distribution table

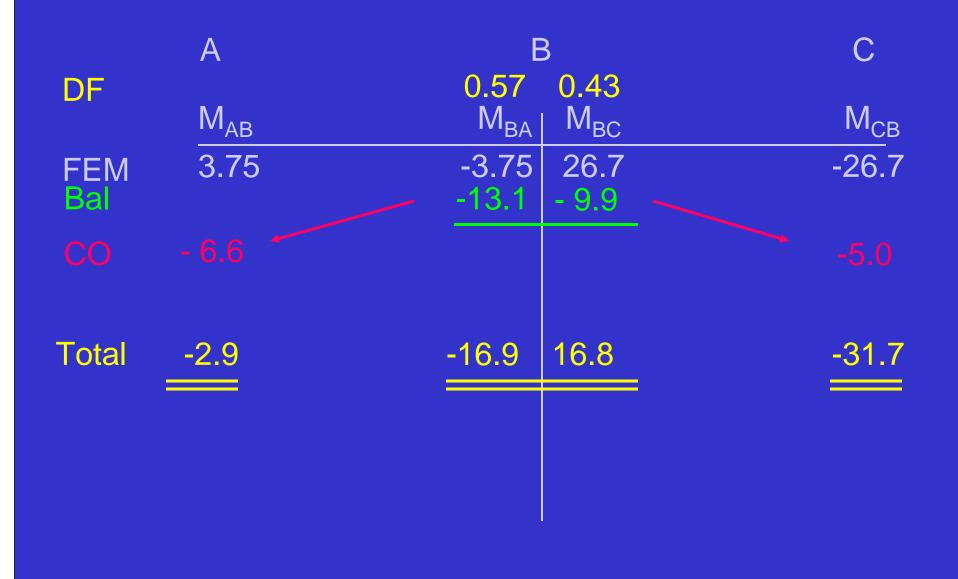
	А		E	3		С
DF	M _{AB}	EI/L	0.57 M _{BA}	0.43 M _{BC}	EI/L	М _{св} -26.7
FEM	3.75		-3.75	26.7		-26.7

Carry out calculations using a moment distribution table

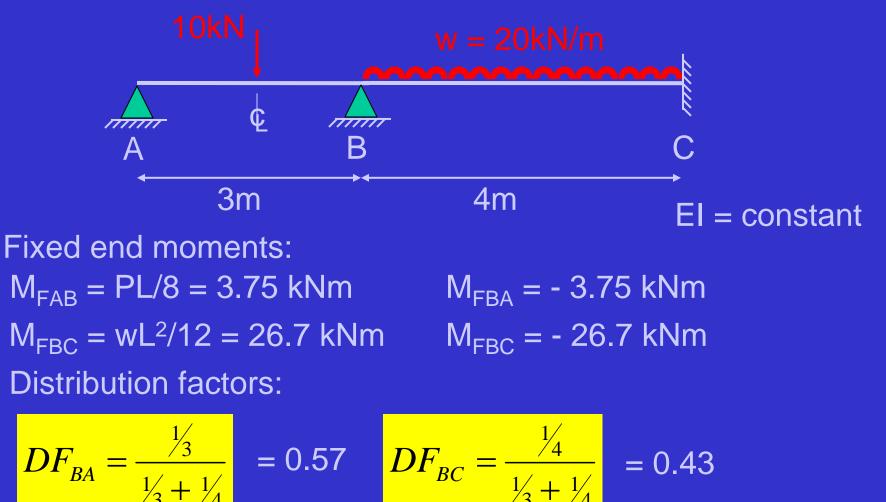




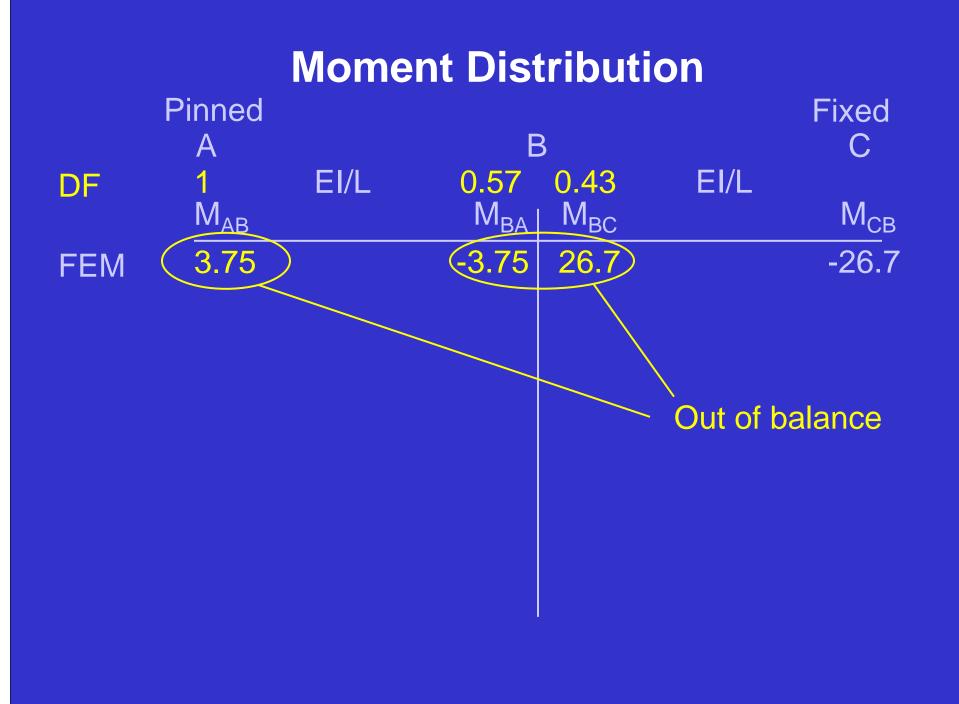




So ... what happens if we replace the fixed support at A with a pinned support ?



Moment Distribution Pinned Fixed В A С EI/L 0.57 EI/L 0.43 1 DF M_{AB} M_{BC} M_{CB} M_{BA} 26.7 3.75 -3.75 -26.7 FEM

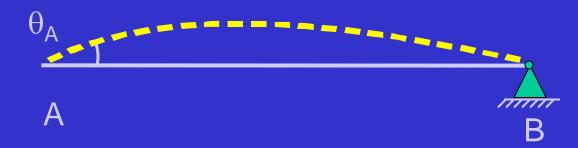


	Pinned			Fixed
	A	E	3	С
DF	1	0.57	0.43	1
	M _{AB}	M _{BA}	M _{BC}	M _{CB}
FEM	3.75	-3.75	-26.7	-26.7
Bal	(-3.75)	<u>(</u> -13.1	-9.9	
			Balancing	
			moments	

	Pinned			Fixed
	A	E	3	С
DF	1	0.57	0.43	1
	M _{AB}	M _{BA}	M _{BC}	M _{CB}
FEM	3.75	-3.75	26.7	-26.7
Bal	-3.75	-13.1	- 9.9 🔶	
	(-6.6)	-1.9		
			er moments	
			or momona	

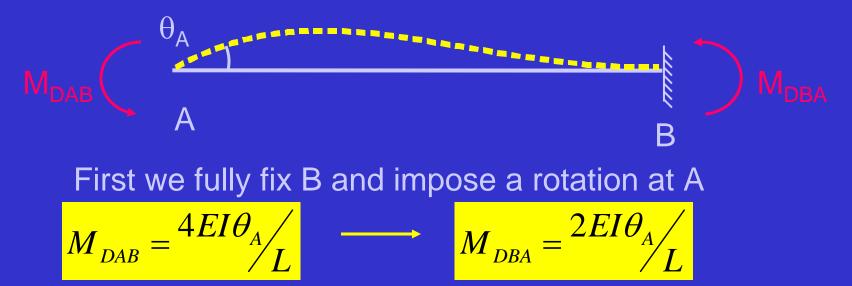
	Pinned A	В	Fixed C
DF	1 M _{AB}	0.57 0.43 M _{BA} M _{BC}	1 M _{CB}
FEM <mark>Bal</mark>	3.75 -3.75	-3.75 26.7 -13.1 - 9.9	-26.7
CO Bal	- 6.6	-1.9 1.1 0.8	
CO Bal	0.6	3.3 - 1.9 - 1.4	
CO Bal	- 1.0	-0.3 0.2 0.1	
CO Bal		0.5 - 0.3 -0.2	
Total	0	- 16.2 16.1	-32.0

You can see that the pin end at A causes a very slow convergence. We can improve on this situation. <u>Consider a beam AB with a rotation at A and B is pinned.</u>

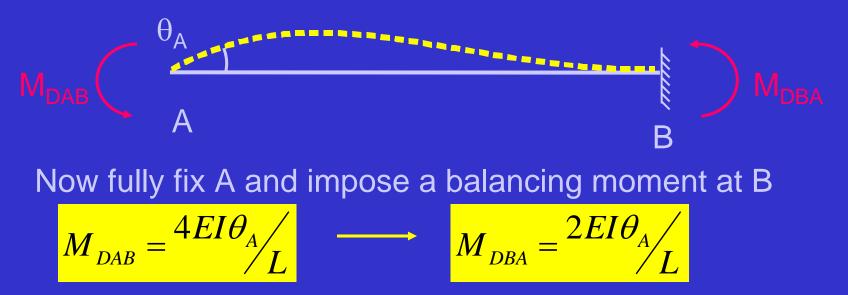


First we fully fix B and impose a rotation at A

You can see that the pin end at A causes a very slow convergence. We can improve on this situation. Consider a beam AB with a rotation at A and B is pinned.

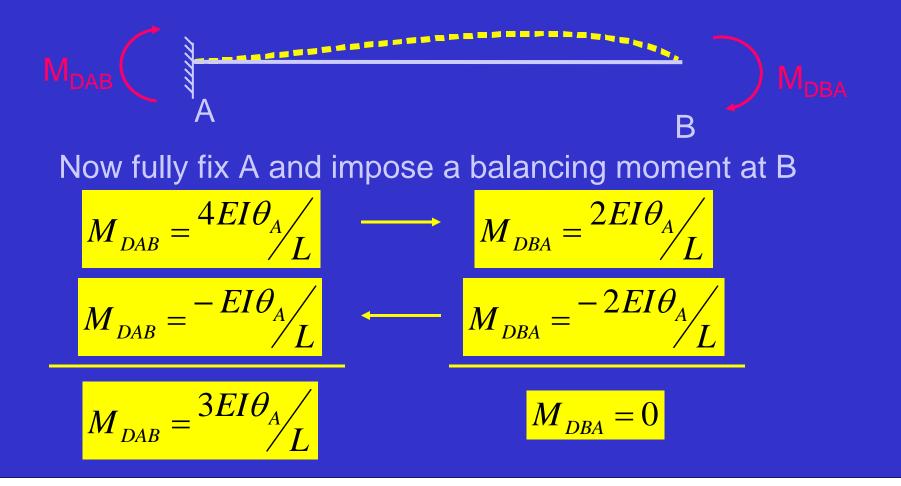


You can see that the pin end at A causes a very slow convergence. We can improve on this situation. Consider a beam AB with a rotation at A and B is pinned.



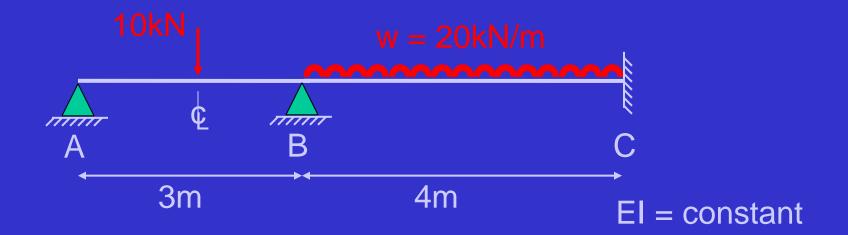
You can see that the pin end at A causes a very slow convergence.

Consider a beam AB with a rotation at A and B is pinned.



So ... if we replace the 4EI/L stiffness of a pin support member with 3EI/L and have a zero carry-over factor, the end result is the same.

Try this with the same problem as before:



=

Distribution factors:

$$DF_{BA} = \frac{\frac{3EI}{L_{AB}}}{\frac{3EI}{L_{AB}} + \frac{4EI}{L_{BC}}} = \frac{3EI}{\frac{3EI}{L_{AB}}}$$

$$\frac{\frac{3}{4\times3}}{\frac{3}{4\times3}+\frac{1}{4}} = 0.5$$

$$DF_{Bc} = \frac{\frac{EI}{L_{BC}}}{\frac{3EI}{4L_{AB}} + \frac{EI}{L_{BC}}}$$

$$\frac{\frac{1}{4}}{\frac{3}{4\times3}+\frac{1}{4}} = 0.5$$

	Pinned A		E	3		Fixed C
DF	1 M _{AB}	0.75EI/L	0.5 M _{BA}	0.5 M _{BC}	EI/L	M _{CB}
FEM Bal	3.75 - <mark>3.75</mark>		-3.75 -11.5	26.7 -11.5		-26.7
	No carry o	over	- 1.9			

	Pinned A		E	3		Fixed C
DF	1 M _{AB}	0.75EI/L	0.5 M _{BA}	0.5 M _{BC}	EI/L	M _{CB}
FEM Bal	3.75 - <mark>3.75</mark>		-3.75 -11.5	26.7 -11.5		-26.7
CO Bal			- 1.9 1.0	1.0		
Total	0		- 16.2	16.2		0.5 -31.8
Total			10.2	10.2		01.0

This is the same result as before.

	Pinned A	В	Fixed C
DF	1 M _{AB}	0.57 0.43 M _{BA} M _{BC}	1 M _{CB}
FEM <mark>Bal</mark>	3.75 -3.75	-3.75 26.7 -13.1 - 9.9	-26.7
CO Bal	- 6.6 6.6	-1.9 1.1 0.8	
CO Bal	0.6	3.3 - 1.9 - 1.4	
CO Bal	- 1.0	-0.3 0.2 0.1	
CO Bal	4	0.5 - 0.3 -0.2	
Total	0	- 16.2 16.1	-32.0