

Stiffness method - Matrix/computer analysis

The Slope-Deflection method generated a series of simultaneous equations, which had to be solved.

This method assumed that the axial extensions of members was very small

We can extend this to include axial stiffnesses/extensions and can write the equations as a matrix equation:

Stiffness method - Matrix/computer analysis

$$\{\text{External Loads}\} = [\text{Stiffness coefficients}] \times \{\text{Joint Displacements}\}$$

where $\{ \}$ is a $n \times 1$ column vector and $[]$ is a $n \times n$ matrix

We can then invert the stiffness matrix to find the unknown displacements.

Matrix inversion is very tedious to do manually, but lends itself to computer solution.

Stiffness method - Matrix/computer analysis

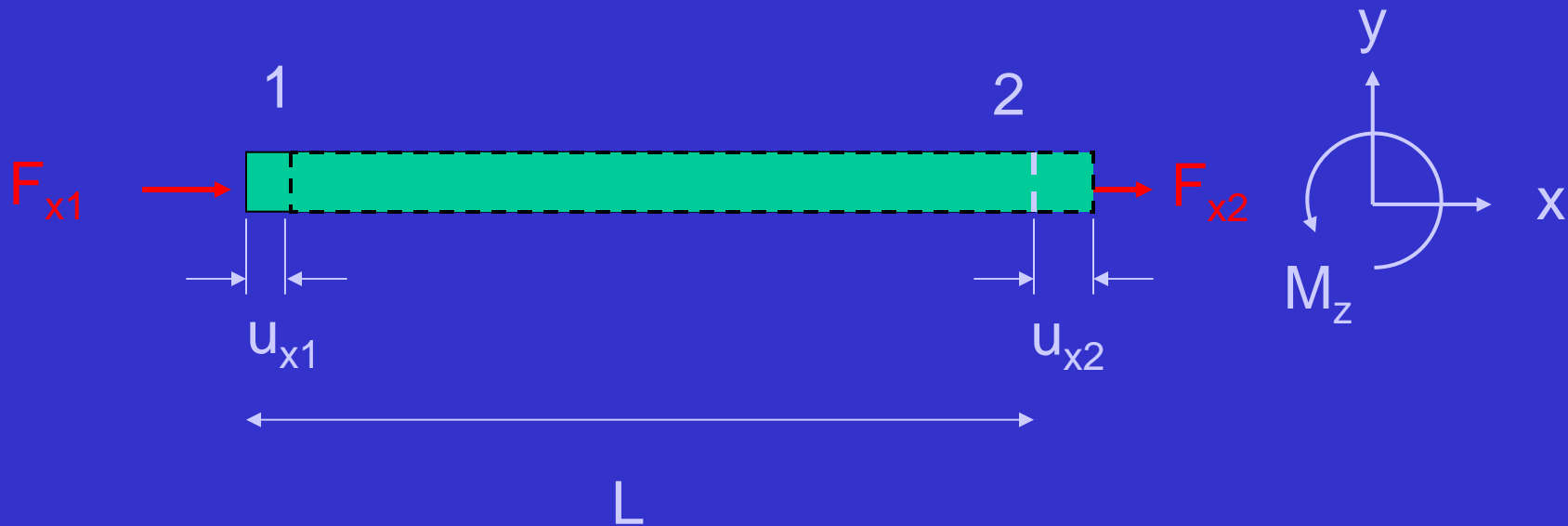
Procedure :

1. Formulate the stiffness matrix for each member, relating forces and displacements at member ends. This is known as the **local stiffness matrix**.
2. Combine the local matrices using conditions of **equilibrium** and **compatibility** to give a **global stiffness matrix** for the whole structure.
3. Invert the stiffness matrix to find the unknown displacements.
4. Substitute displacements back into local stiffness matrix to find member forces.

Stiffness method - Matrix/computer analysis

We can demonstrate this method using a simple example of an axially loaded member.

1. Formulate the **local stiffness matrix**.



Now consider each displacement separately:

$$F_{x1} = \frac{AE}{L} u_{x1}$$

$$F_{x2} = -\frac{AE}{L} u_{x1}$$

$$F_{x1} = -\frac{AE}{L} u_{x2}$$

$$F_{x2} = \frac{AE}{L} u_{x2}$$

Stiffness method - Matrix/computer analysis

Use **Principle of Superposition** to find forces when displacements act simultaneously.

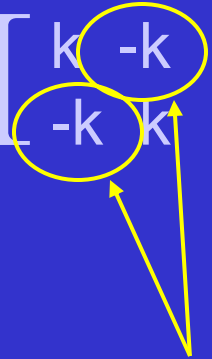
$$\begin{Bmatrix} F_{x1} \\ F_{x2} \end{Bmatrix} = \begin{bmatrix} k & -k \\ -k & k \end{bmatrix} \begin{Bmatrix} u_{x1} \\ u_{x2} \end{Bmatrix}$$

where $k = AE/L$

Leading diagonal terms relate forces and displacements at same end and in same direction.

Stiffness method - Matrix/computer analysis

Use **Principle of Superposition** to find forces when displacements act simultaneously.

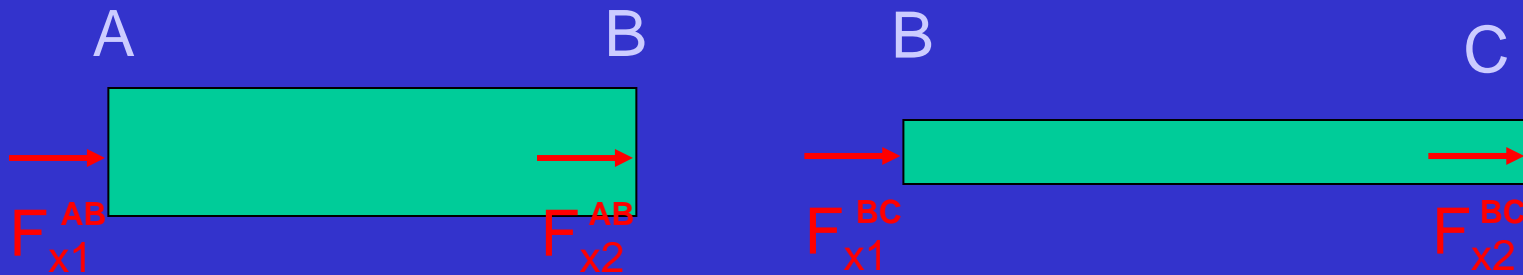
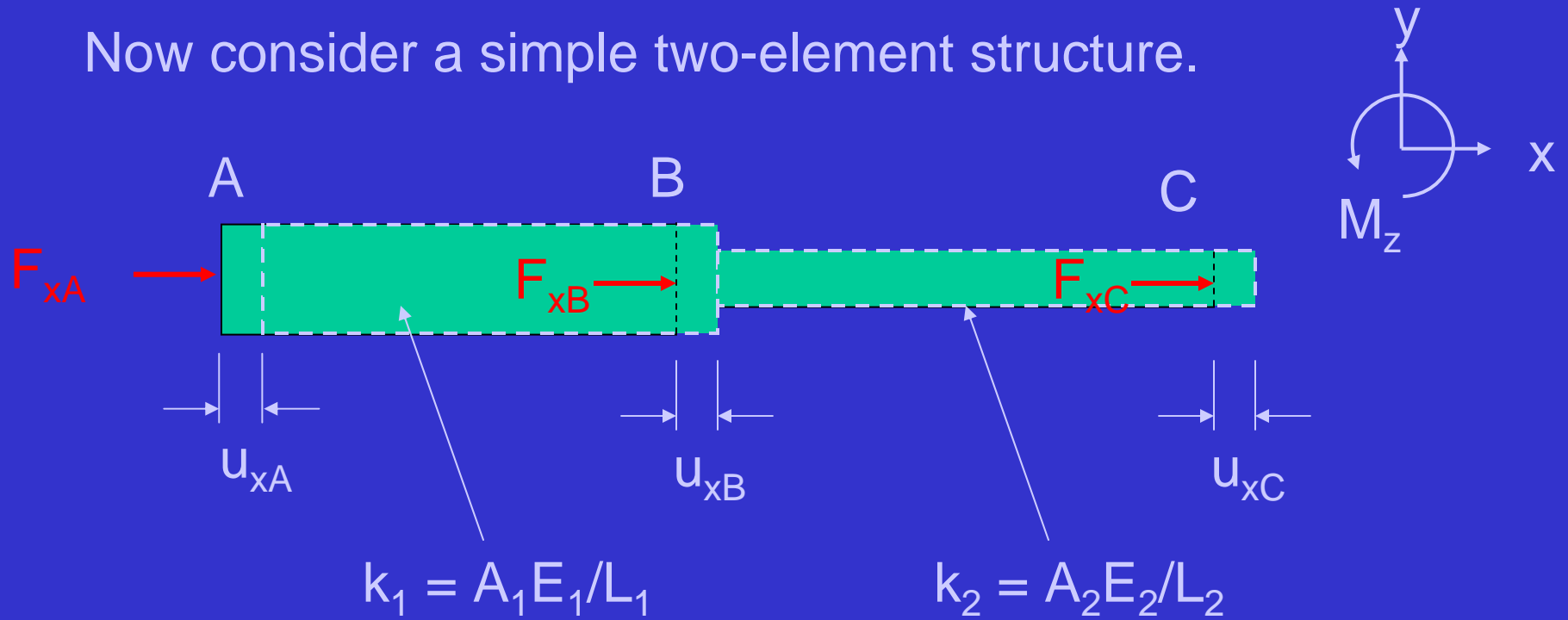
$$\begin{Bmatrix} F_{x1} \\ F_{x2} \end{Bmatrix} = \begin{bmatrix} k & -k \\ -k & k \end{bmatrix} \begin{Bmatrix} u_{x1} \\ u_{x2} \end{Bmatrix}$$
The diagram shows the stiffness matrix $\begin{bmatrix} k & -k \\ -k & k \end{bmatrix}$ with the off-diagonal terms $-k$ circled in yellow. Two yellow arrows originate from these circles and point towards the text box below.

where $k = AE/L$

Off-diagonal terms relate forces and displacements to cross-coupled ends

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Now consider a simple two-element structure.



Stiffness method - Matrix/computer analysis

For AB: local stiffness matrix

$$\begin{Bmatrix} F_{x1}^{AB} \\ F_{x2}^{AB} \end{Bmatrix} = \begin{bmatrix} k_1 & -k_1 \\ -k_1 & k_1 \end{bmatrix} \begin{Bmatrix} u_{x1}^{AB} \\ u_{x2}^{AB} \end{Bmatrix}$$

For BC: local stiffness matrix

$$\begin{Bmatrix} F_{x1}^{BC} \\ F_{x2}^{BC} \end{Bmatrix} = \begin{bmatrix} k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{Bmatrix} u_{x1}^{BC} \\ u_{x2}^{BC} \end{Bmatrix}$$

1. Formulate the **local stiffness matrices**.

Stiffness method - Matrix/computer analysis

Compatibility :

$$u_{x1}^{AB} = u_{xA}$$

$$u_{x2}^{AB} = u_{x1}^{BC} = u_{xB}$$

$$u_{x2}^{BC} = u_{xC}$$

$$\begin{Bmatrix} F_{x1}^{AB} \\ F_{x2}^{AB} \end{Bmatrix} = \begin{bmatrix} k_1 & -k_1 \\ -k_1 & k_1 \end{bmatrix} \begin{Bmatrix} u_{xA} \\ u_{xB} \end{Bmatrix}$$

$$\begin{Bmatrix} F_{x1}^{BC} \\ F_{x2}^{BC} \end{Bmatrix} = \begin{bmatrix} k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{Bmatrix} u_{xB} \\ u_{xC} \end{Bmatrix}$$

2. Use equilibrium and compatibility to find **global stiffness matrix**

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Equilibrium :

$$\begin{Bmatrix} F_{xA} \\ F_{xB} \\ F_{xC} \end{Bmatrix} = \begin{Bmatrix} F_{x1} \\ F_{x2} \\ 0 \end{Bmatrix}_{AB} + \begin{Bmatrix} 0 \\ F_{x1} \\ F_{x2} \end{Bmatrix}_{BC}$$

Hence

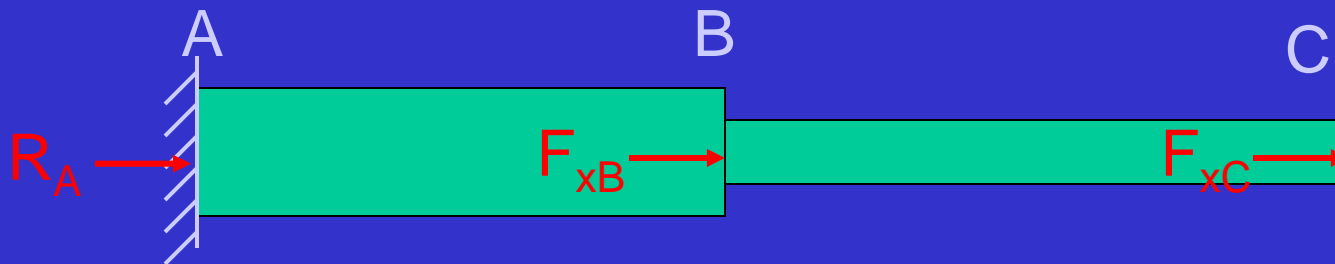
$$\begin{Bmatrix} F_{xA} \\ F_{xB} \\ F_{xC} \end{Bmatrix} = \begin{bmatrix} k_1 & -k_1 & 0 \\ -k_1 & k_1 + k_2 & -k_2 \\ 0 & -k_2 & k_2 \end{bmatrix} \begin{Bmatrix} u_{xA} \\ u_{xB} \\ u_{xC} \end{Bmatrix}$$

2. Use equilibrium and compatibility to find **global stiffness matrix**

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We cannot yet invert the stiffness matrix because it is singular. i.e. we will get $0 = 0$!

This is because the structure has no **Boundary Conditions**. It is floating in space...!



If we fix the structure at A :

$$F_{xA} = R_A \quad \text{and} \quad u_{xA} = 0$$

3. Invert the stiffness matrix to find the unknown displacements.

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$$\begin{Bmatrix} R_A \\ F_{xB} \\ F_{xC} \end{Bmatrix} = \begin{bmatrix} k_1 & -k_1 & 0 \\ -k_1 & k_1 + k_2 & -k_2 \\ 0 & -k_2 & k_2 \end{bmatrix} \begin{Bmatrix} 0 \\ u_{xB} \\ u_{xC} \end{Bmatrix}$$

The 1st column of the stiffness matrix is multiplied by zero & plays no part. The stiffness matrix reduces to:

$$\begin{Bmatrix} F_{xB} \\ F_{xC} \end{Bmatrix} = \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{Bmatrix} u_{xB} \\ u_{xC} \end{Bmatrix}$$

3. Invert the stiffness matrix to find the unknown displacements.

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Inverting the stiffness matrix gives :

$$\begin{Bmatrix} u_{xB} \\ u_{xC} \end{Bmatrix} = 1/k_1k_2 \begin{bmatrix} k_2 & k_2 \\ k_2 & k_1 + k_2 \end{bmatrix} \begin{Bmatrix} F_{xB} \\ F_{xC} \end{Bmatrix}$$

Hence u_{xB} & u_{xC} are found

3. Invert the stiffness matrix to find the unknown displacements.