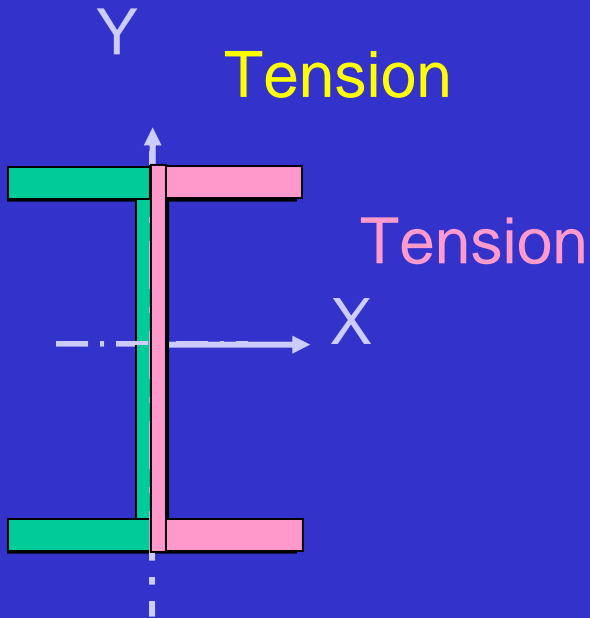


# Biaxial bending of asymmetric section



Define +ve  $M_x$  as causing +ve tensile stresses when  $y$  is +ve

Define +ve  $M_y$  as causing +ve tensile stresses when  $x$  is +ve

# Biaxial bending of asymmetric section

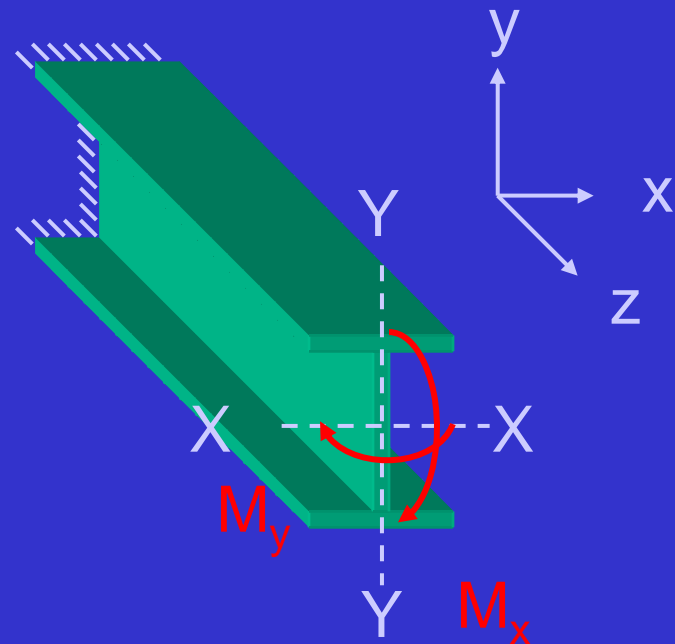
What happens if we try and bend an asymmetric section without applying the load at the shear centre?

For the case of biaxial bending of symmetric section:

+ve  $M_y$  gives +ve tension on +ve X side of section

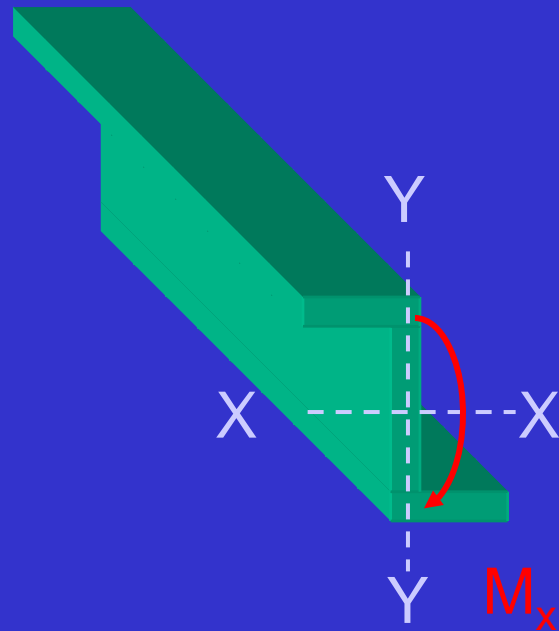
$$\sigma_z = \frac{M_x y}{I_{xx}} + \frac{M_y x}{I_{yy}}$$

+ve  $M_x$  gives +ve tension on +ve Y side of section

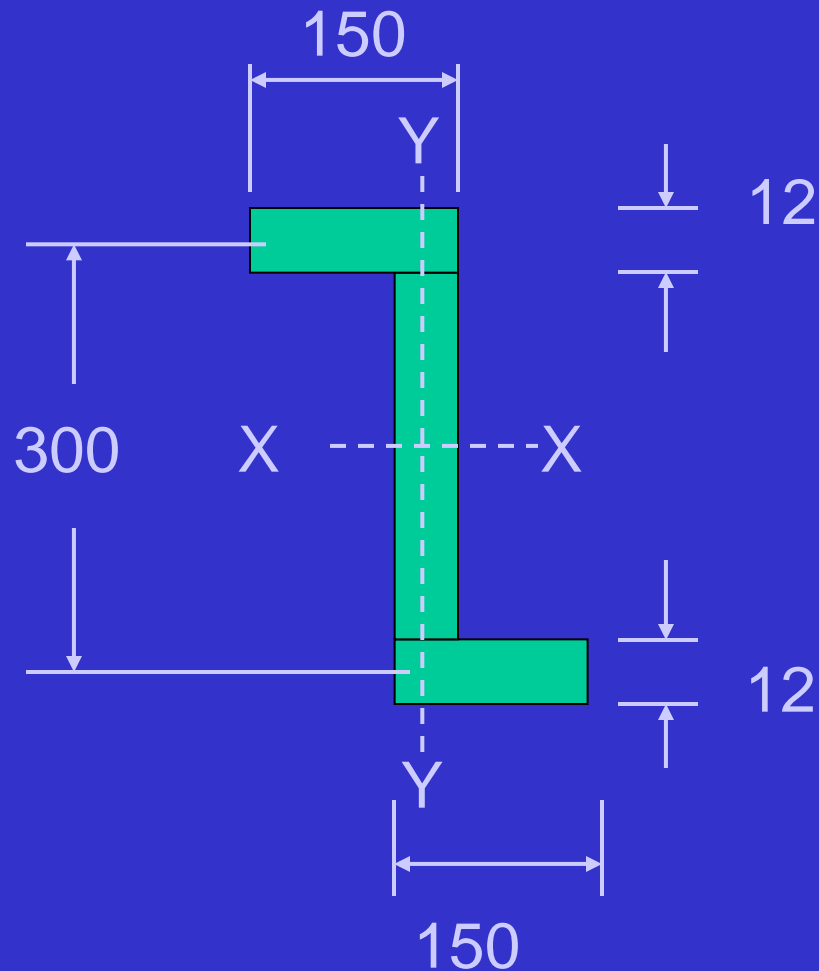


# Biaxial bending of asymmetric section

What happens if we try and apply the same equation to an asymmetric section for a moment  $M_x$  ?



# Biaxial bending of asymmetric section



$$I_{xx} = 95.7 \times 10^6 \text{ mm}^4$$

$$I_{yy} = 23.9 \times 10^6 \text{ mm}^4$$

Now apply a hogging (positive) bending moment of  $M_x = 10 \text{ kN.m} = 10 \times 10^6 \text{ N.mm}$

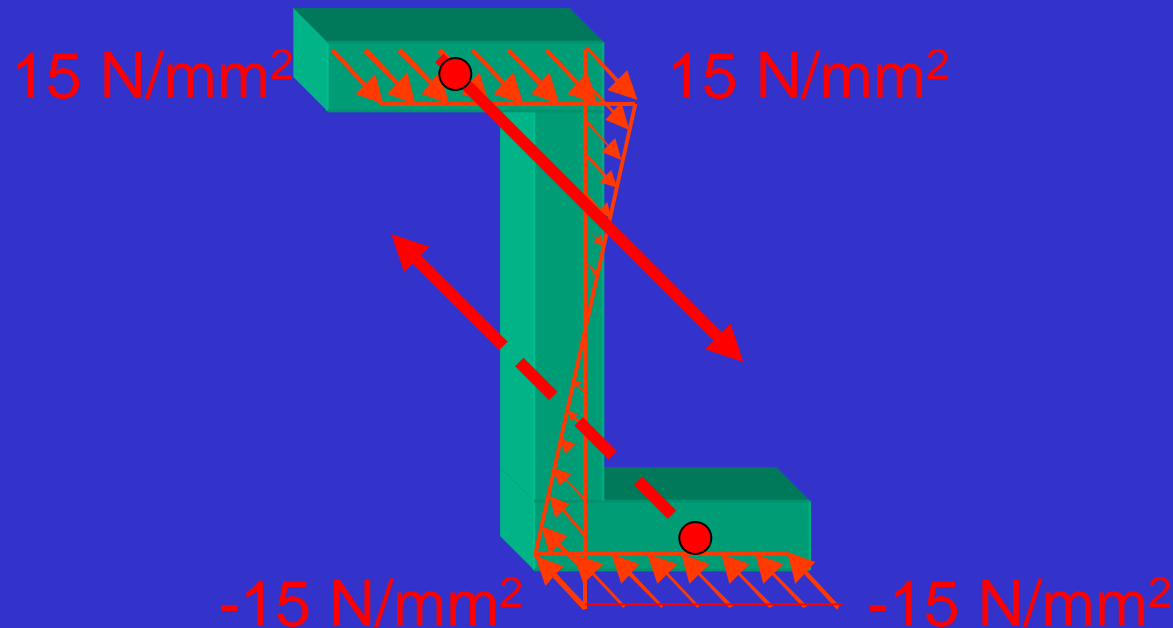
# Biaxial bending of asymmetric section

$$\sigma_z = \frac{M_x y}{I_{xx}} + \frac{M_y x}{I_{yy}} = 0.105 y \text{ N.mm}^{-3}$$

The average stress in the top flange at  $y = 144 \text{ mm}$  is  $\sigma_z = 15 \text{ N/mm}^2$  (tension positive)

Similarly the average stress in the bottom flange at  $y = -144 \text{ mm}$  is  $\sigma_z = -15 \text{ N/mm}^2$  (compression negative)

# Biaxial bending of asymmetric section



The forces in the flanges result in horizontal forces that are laterally out of alignment.

This result in a lateral bending moment about the Y-Y axis... and yet there is no external  $M_y$  moment applied !



Although only  $M_x$  is applied, the section must bend about Y-Y

# Biaxial bending of asymmetric section

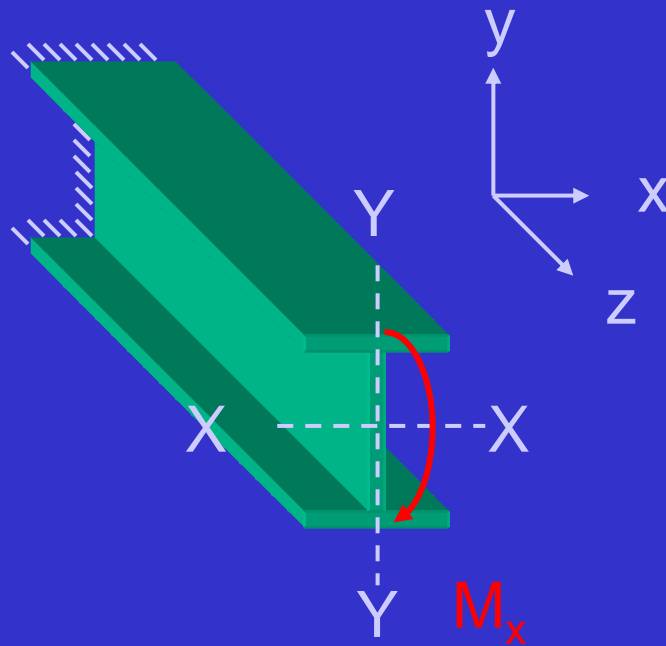
General expression for bending stress

For simple bending  $M_x$  of a section symmetric about the Y-Y axis, axial displacement at any section (in the Z direction) is given by:

$$u = C y$$

and the axial strain is given by:

$$\varepsilon_z = \frac{du}{dz}$$



# Biaxial bending of asymmetric section

General expression for bending stress

For an asymmetric section, we must replace this function for  $u$  by a more general expression:

$$u = C_1 y + C_2 x$$

$$\text{now } \varepsilon_z = \frac{du}{dz} = C'_1 y + C'_2 x$$

$$\text{where } C'_1 = \frac{dC_1}{dz} \quad \text{and} \quad C'_2 = \frac{dC_2}{dz}$$

$$\text{Note : } \sigma_z = E \varepsilon_z$$

$$\text{hence } \sigma_z = E.C'_1.y + E.C'_2.x$$



# Biaxial bending of asymmetric section

Moment about the x axis =  $M_x$

$$M_x = \int \sigma_z y dA = EC'_1 \int y^2 dA + EC'_2 \int xy dA$$

Moment about the y axis =  $M_y$

$$M_y = \int \sigma_z x dA = EC'_1 \int xy dA + EC'_2 \int x^2 dA$$

# Biaxial bending of asymmetric section

Define :

$$\int y^2 dA = I_{xx} \quad = \text{second moment of area about the x axis}$$

$$\int x^2 dA = I_{yy} \quad = \text{second moment of area about the y axis}$$

$$\int xy dA = I_{xy} \quad = \text{cross second moment of area about the x-y axes}$$

$I_{xy}$  is also known as the **product moment of area**

# Biaxial bending of asymmetric section

Hence: 
$$M_x = EC'_1 I_{xx} + EC'_2 I_{xy}$$

$$M_y = EC'_1 I_{xy} + EC'_2 I_{yy}$$

Solving for  $C'_1$  and  $C'_2$  gives:

$$EC'_1 = \frac{(M_x I_{yy} - M_y I_{xy})}{(I_{yy} I_{xx} - I_{xy}^2)}$$

$$EC'_2 = \frac{(-M_x I_{xy} + M_y I_{xx})}{(I_{yy} I_{xx} - I_{xy}^2)}$$

# Biaxial bending of asymmetric section

$$\sigma_z = EC'_1 y + EC'_2 x$$

$$\sigma_z = \frac{(M_x I_{yy} - M_y I_{xy})}{(I_{yy} I_{xx} - I_{xy}^2)} y + \frac{(-M_x I_{xy} + M_y I_{xx})}{(I_{yy} I_{xx} - I_{xy}^2)} x$$

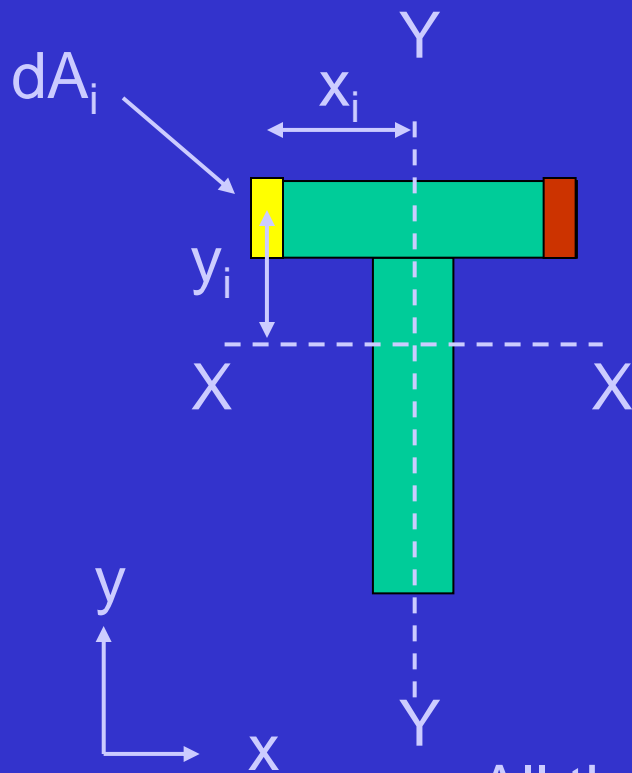
Note that if  $I_{xy} = 0$ ,

$$\sigma_z = \frac{M_x}{I_{xx}} y + \frac{M_y}{I_{yy}} x$$

This is the same formula as used for a symmetric section

# Biaxial bending of asymmetric section

Why is  $I_{xy} = 0$  for a symmetric section ?



$$I_{xy} = \int xy \, dA$$

$$I_{xy} = \sum x_i y_i dA_i$$

For every area  $dA_i$  with location +ve  $y$ , -ve  $x$  there is a corresponding area  $dA_i$  with location +ve  $y$ , +ve  $x$

All the contributions to  $\sum x_i y_i dA_i$  will cancel out

# Biaxial bending of asymmetric section

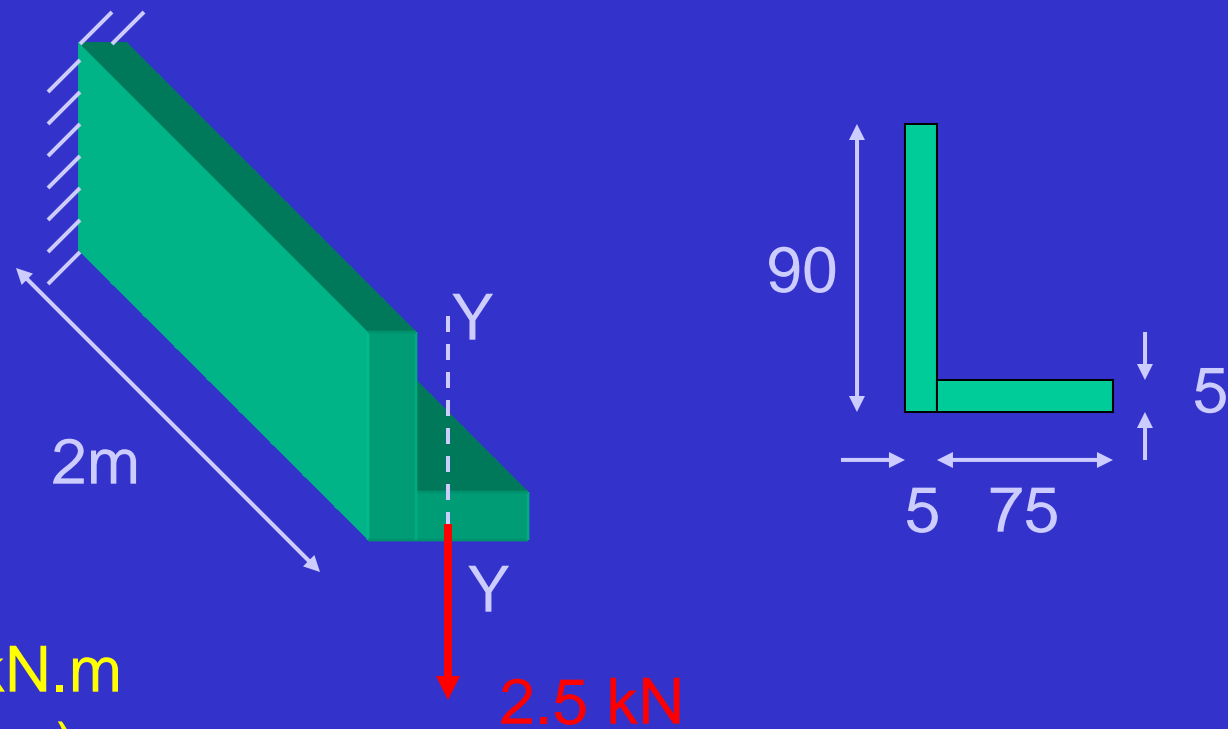
For a section with at least one axis of symmetry  
about X-X or Y-Y:

$$I_{xy} = 0$$

# Biaxial bending of asymmetric section

Example:

The L-section cantilever shown has a point load of 2.5 kN applied at the tip of the cantilever. The load is applied at the centroidal Y-Y axis. What are the bending stresses ?



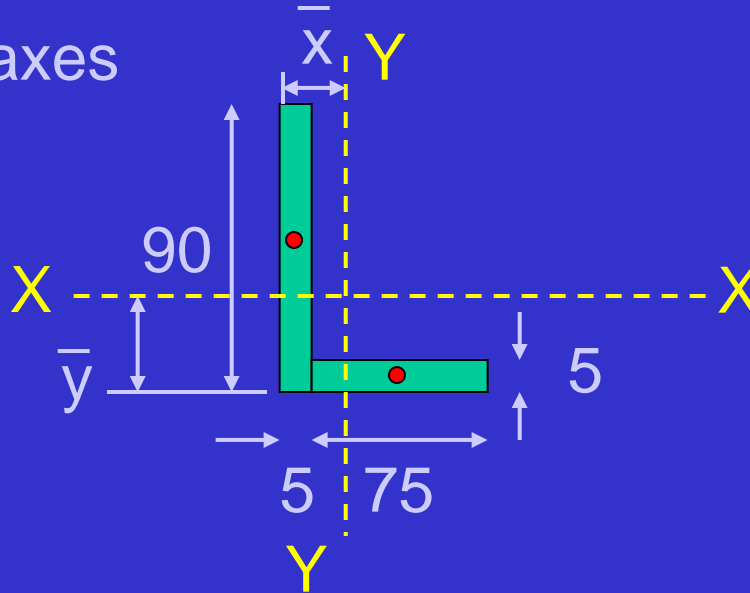
$$M_x = 5.0 \text{ kN.m}$$

(hogging +ve)

2.5 kN

# Biaxial bending of asymmetric section

Find the centroidal axes



$$\text{Total area} = 90 \times 5 + 75 \times 5 = 825 \text{ mm}^2$$

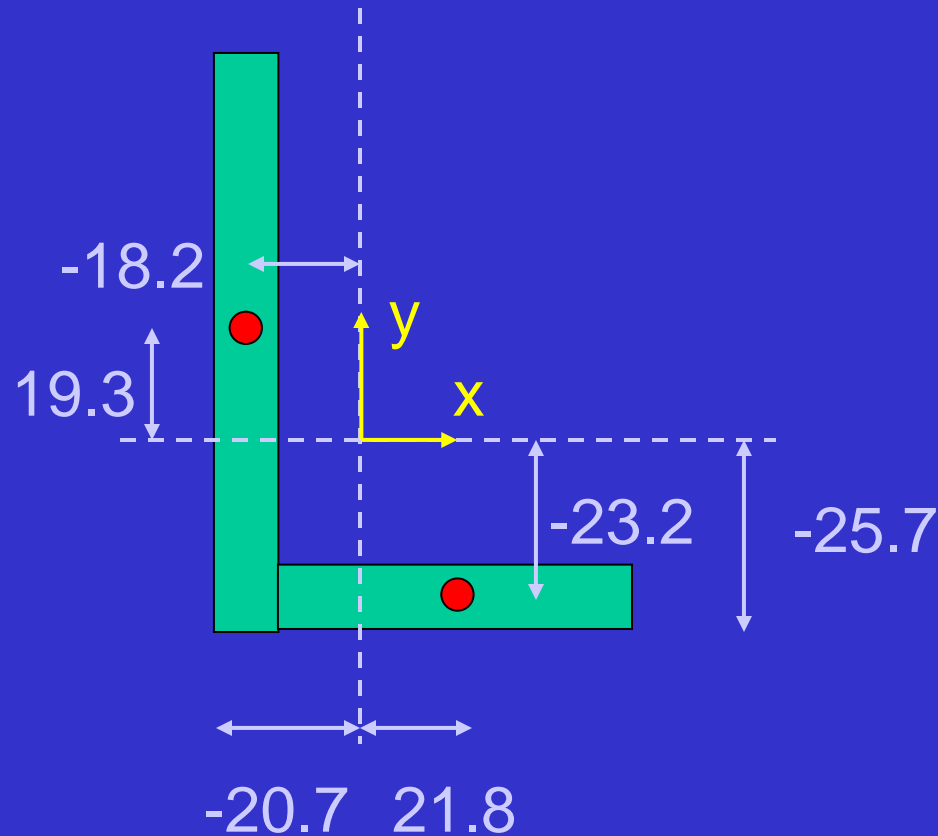
$$\bar{y} = \frac{(90 \times 5 \times 45) + (75 \times 5 \times 2.5)}{825} = 25.7 \text{ mm}$$

$$\bar{x} = \frac{(90 \times 5 \times 2.5) + (75 \times 5 \times 42.5)}{825} = 20.7 \text{ mm}$$



# Biaxial bending of asymmetric section

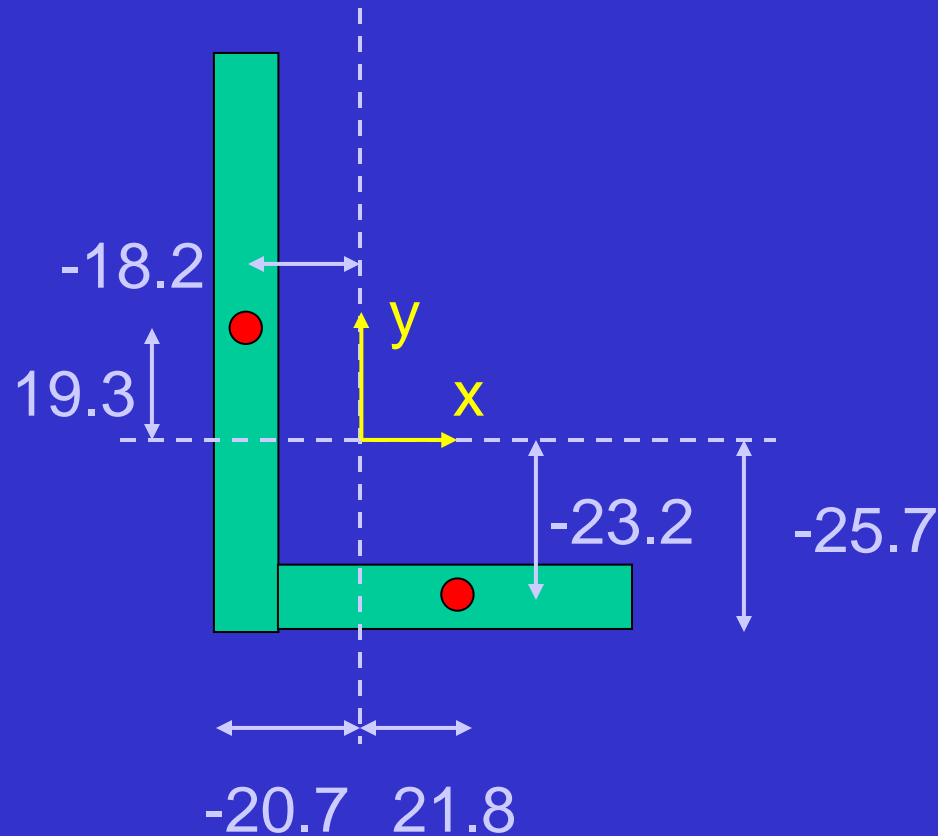
Now find  $I_{xx}$ ,  
 $I_{yy}$  and  $I_{xy}$   
about the  
centroidal axes



$$I_{xx} = \frac{5 \times 90^3}{12} + (5 \times 90 \times 19.3^2) + \frac{75 \times 5^3}{12} + (5 \times 75 \times -23.2^2)$$

$$I_{xx} = 673991 \text{ mm}^4 = 6.74 \times 10^5 \text{ mm}^4$$

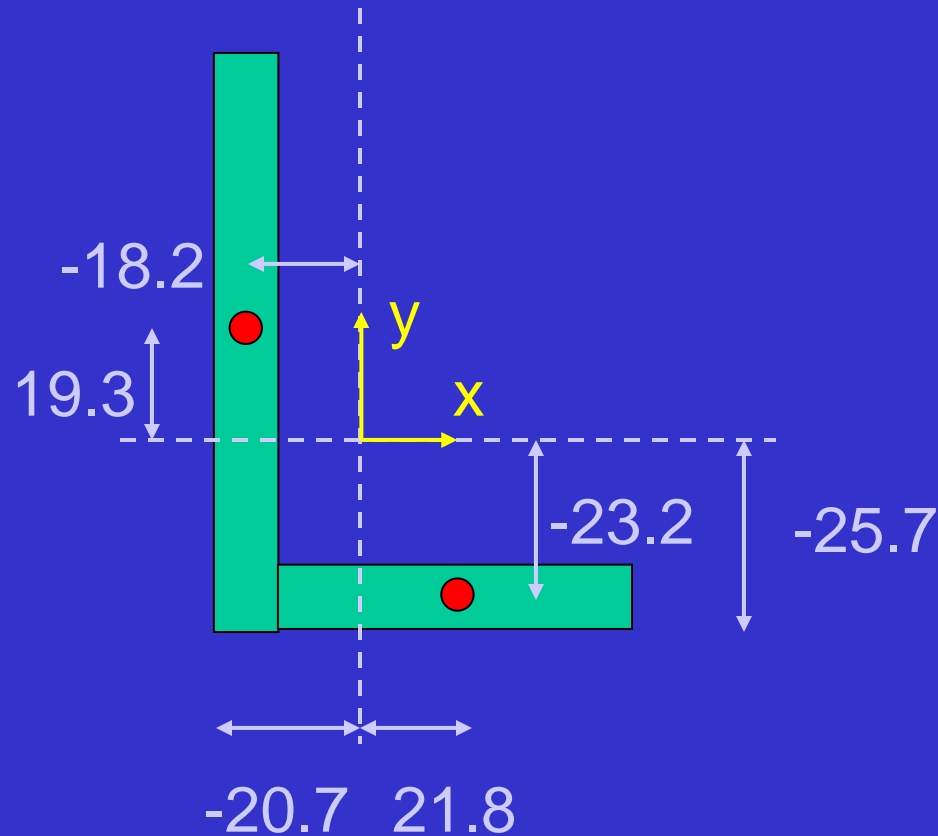
# Biaxial bending of asymmetric section



$$I_{yy} = \frac{90 \times 5^3}{12} + (5 \times 90 \times -18.2^2) + \frac{5 \times 75^3}{12} + (5 \times 75 \times 21.8^2)$$

$$I_{yy} = 503991 \text{ mm}^4 = 5.04 \times 10^5 \text{ mm}^4$$

# Biaxial bending of asymmetric section



$$I_{xy} = (5 \times 90 \times -18.2 \times 19.3) + (5 \times 75 \times -23.2 \times 21.8)$$

$$I_{xy} = -347727 \text{ mm}^4 = -3.48 \times 10^5 \text{ mm}^4$$

# Biaxial bending of asymmetric section

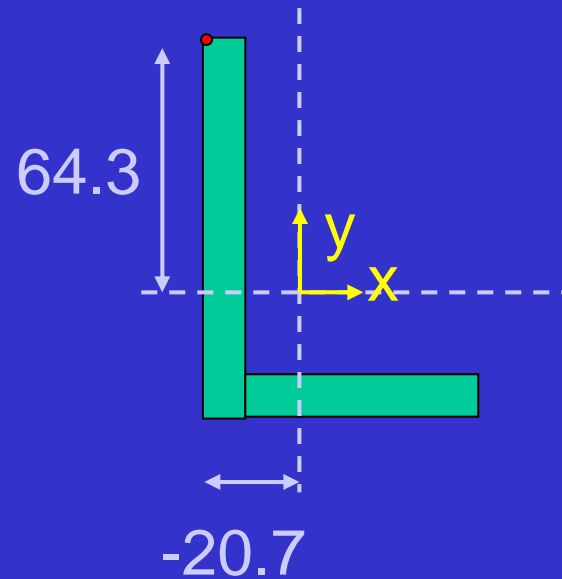
$$\sigma_z = \frac{(M_x I_{yy} - \cancel{M_y I_{xy}})}{(I_{yy} I_{xx} - I_{xy}^2)} y + \frac{(-M_x I_{xy} + \cancel{M_y I_{xx}})}{(I_{yy} I_{xx} - I_{xy}^2)} x$$

Hogging +ve, tension +ve

$$M_x = 5.0 \text{ kN.m}, M_y = 0$$

# Biaxial bending of asymmetric section

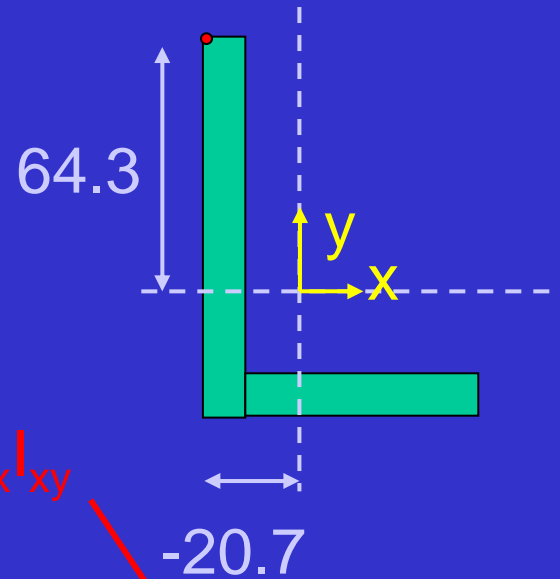
Top-left corner



$$\sigma_z = \frac{(5 \times 10^6 \times 5.04 \times 10^5)}{(5.04 \times 6.74 - 3.48^2) \times 10^{10}} \times 64.3$$
$$+ \frac{(-5 \times 10^6 \times [-3.45 \times 10^5])}{(5.04 \times 6.74 - 3.48^2) \times 10^{10}} \times [-20.7]$$

# Biaxial bending of asymmetric section,

Top-left corner



$M_x I_{yy}$

$M_x I_{xy}$

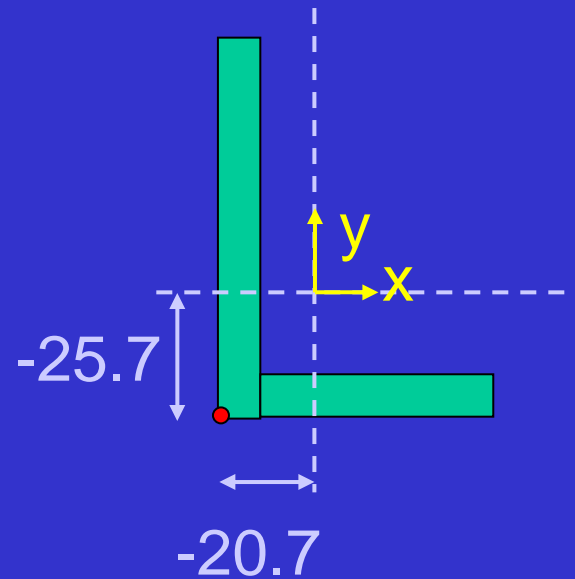
$$\sigma_z = \frac{2.52 \times 10^{12}}{2.20 \times 10^{11}} \times 64.3 + \frac{1.73 \times 10^{12}}{2.20 \times 10^{11}} \times [-20.7]$$

$I_{xx} I_{yy} - I_{xy}^2$

$$\sigma_z = 738 - 163 = 575 \text{ N/mm}^2$$

# Biaxial bending of asymmetric section

Bottom-left corner

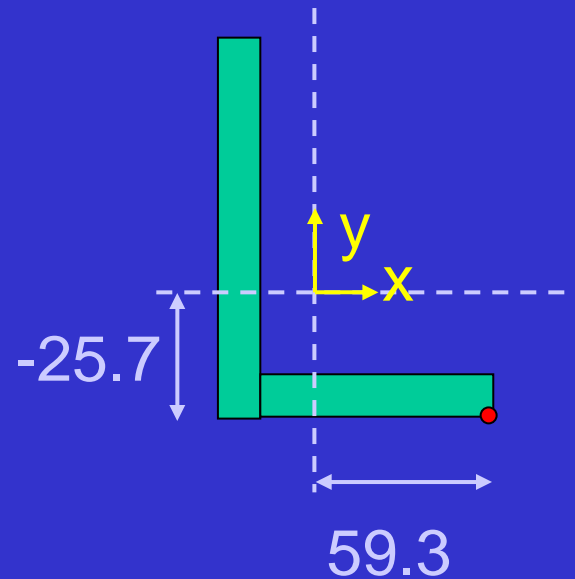


$$\sigma_z = \frac{2.52 \times 10^{12}}{2.20 \times 10^{11}} \times [-25.7] + \frac{1.73 \times 10^{12}}{2.20 \times 10^{11}} \times [-20.7]$$

$$\sigma_z = -295 - 163 = -458 \text{ N/mm}^2$$

# Biaxial bending of asymmetric section

Bottom-right corner

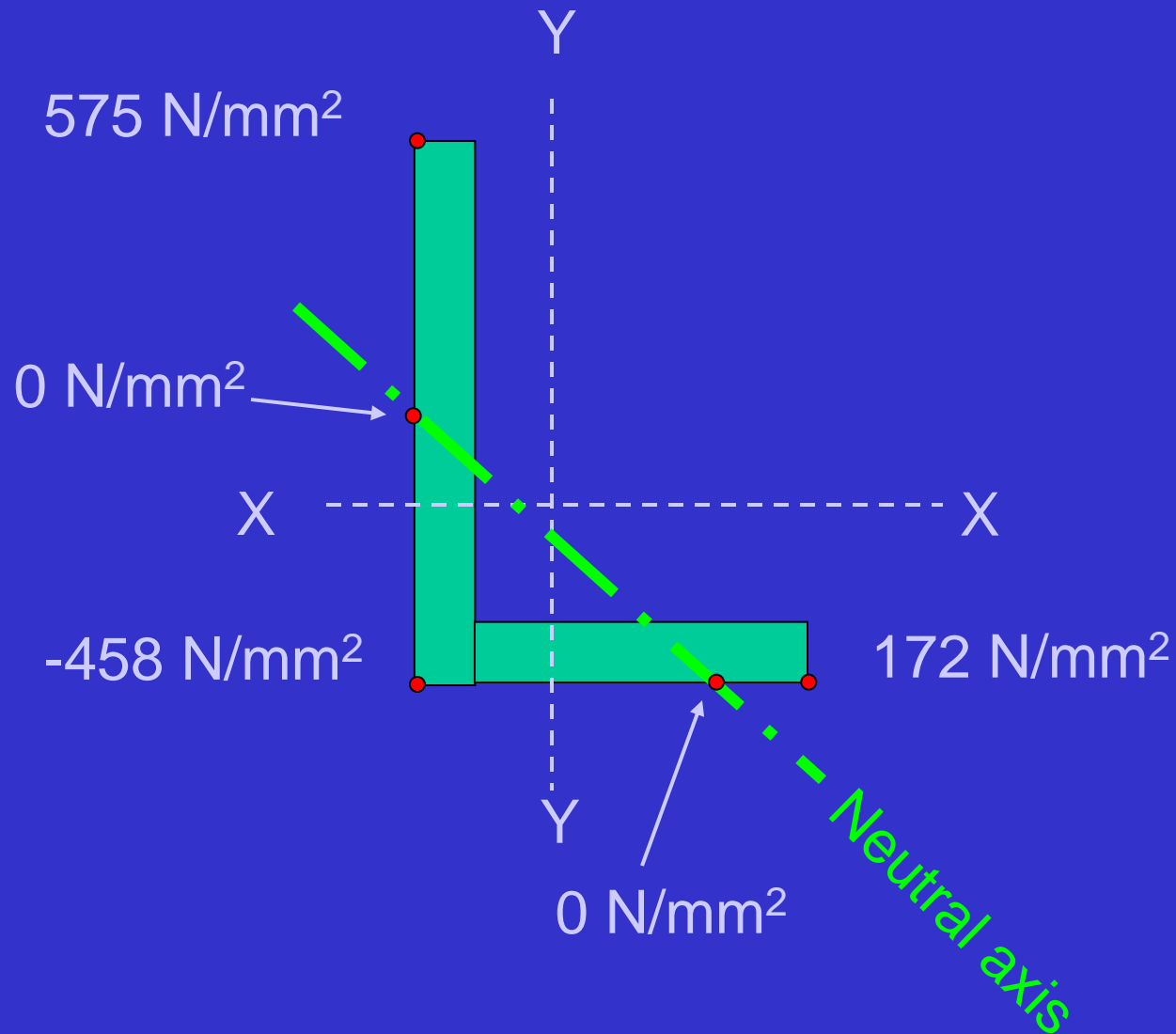


$$\sigma_z = \frac{2.52 \times 10^{12}}{2.20 \times 10^{11}} \times [-25.7] + \frac{1.73 \times 10^{12}}{2.20 \times 10^{11}} \times 59.3$$

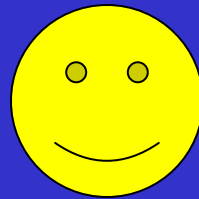
$$\sigma_z = -295 + 467 = 172 \text{ N/mm}^2$$



# Biaxial bending of asymmetric section



# Biaxial bending of asymmetric section



Alternative method ...

# Biaxial bending of asymmetric section

It can be shown that we can use the symmetric equation

$$\sigma_z = \frac{M_x}{I_{xx}} y + \frac{M_y}{I_{yy}} x$$

for asymmetric sections, if we replace  $M_x$  and  $M_y$  by  $\overline{M}_x$  and  $\overline{M}_y$ , where :

$$\overline{M}_x = \frac{M_x - M_y \times I_{xy} / I_{xx}}{1 - I_{xy}^2 / (I_{xx} I_{yy})}$$

$$\overline{M}_y = \frac{M_y - M_x \times I_{xy} / I_{yy}}{1 - I_{xy}^2 / (I_{xx} I_{yy})}$$

# Biaxial bending of asymmetric section

In the example:  $M_x = 5.0 \text{ kN.m}$ ,  $M_y = 0$

$$I_{xx} = 6.74 \times 10^5 \text{ mm}^4 \quad I_{yy} = 5.04 \times 10^5 \text{ mm}^4$$

$$I_{xy} = -3.48 \times 10^5 \text{ mm}^4$$

$$\overline{M}_x = \frac{5.0}{1 - [-3.48]^2 / (6.74 \times 5.04)} = 7.77 \text{ kN.m}$$

$$\overline{M}_y = \frac{-5.0 \times [-3.48 / 6.74]}{1 - [-3.48]^2 / (6.74 \times 5.04)} = 4.01 \text{ kN.m}$$

Note: even though the applied  $M_y = 0$ , there is an effective bending  $M_y$  for an asymmetric section !

# Biaxial bending of asymmetric section

$$\sigma_z = \frac{\overline{M}_x}{I_{xx}} y + \frac{\overline{M}_y}{I_{yy}} x$$

For top left corner

$$\sigma_z = \frac{7.77 \times 10^6}{6.74 \times 10^5} \times 64.3 + \frac{4.01 \times 10^6}{5.05 \times 10^5} \times [-20.7]$$

$$\sigma_z = 741 - 164$$

Same solution as before

